

$$\langle \phi \rangle = \int d^3p \phi f^0(\vec{p}) / \int d^3p f^0(\vec{p})$$

$$= \int d^3v P(\vec{v}) \phi ; P(\vec{v}) = \left( \frac{m}{2\pi k_B T} \right)^{3/2} e^{-m\vec{v}^2/2k_B T}$$

Here  $T$  is the avg temperature since  $\vec{j}_\varepsilon \propto \vec{\nabla} T$ .

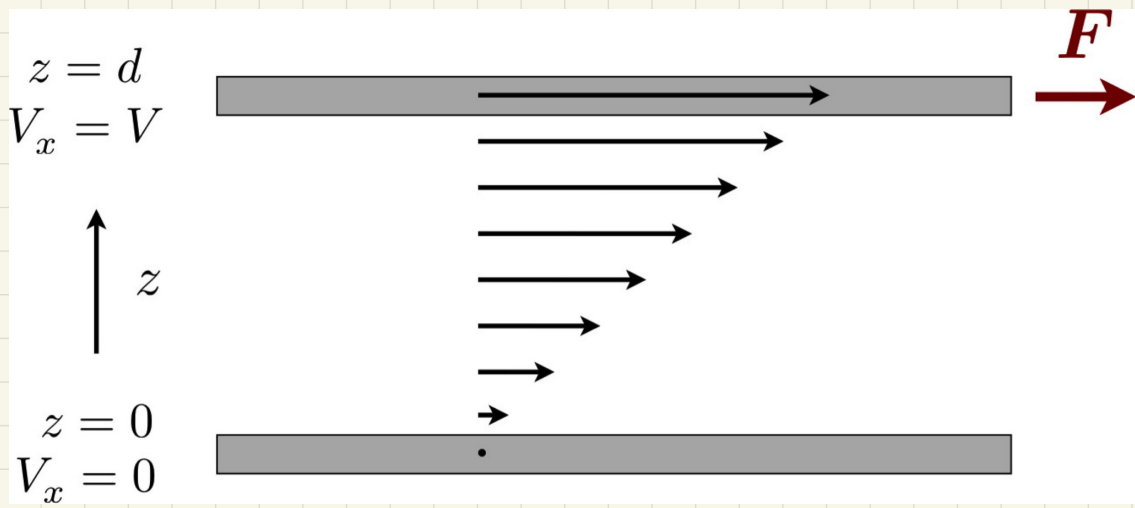
If  $\phi = \phi(\varepsilon)$ , we can use  $P(\vec{v})d^3v = \mathcal{P}(\varepsilon)d\varepsilon$   
 with  $\mathcal{P}(\varepsilon) = \frac{2}{\sqrt{\pi}} (k_B T)^{-3/2} \varepsilon^{1/2} e^{-\varepsilon/k_B T}$ . Then  
 find  $\langle \varepsilon^\theta \rangle = \frac{2}{\sqrt{\pi}} \Gamma(\theta + \frac{3}{2}) (k_B T)^\theta$ . Thus

$$\vec{j}_\varepsilon = -\kappa \vec{\nabla} T, \text{ with thermal conductivity}$$

$$\kappa = \frac{2n\tau}{3mk_B T^2} \langle \varepsilon^2 (\varepsilon - \frac{5}{2} k_B T) \rangle = \frac{5n\tau k_B^2 T}{2m} = \frac{\pi}{8} n l \bar{v} C_p$$

## Viscosity

Consider the situation depicted in the figure below. A fluid between two plates is sheared by applying a horizontal force to the upper plate. The lower plate is held fixed.



If the top plate moves at velocity  $V\hat{x}$ , what force  $F\hat{x}$  must be applied? Fluid particles next to the top plate have average momentum  $\langle p_x \rangle = mV$ . As they move downward, they carry their  $\hat{x}$ -momentum with them, away from the top plate. Particles from below take their place and must be accelerated to  $\langle \vec{v} \rangle = V\hat{x}$ , resulting in a viscous drag on the upper plate,  $\vec{F}_{\text{drag}}$ , in the  $-\hat{x}$  direction. Thus  $\vec{F} = -\vec{F}_{\text{drag}}$ . The momentum density injected into the fluid at the upper plate is then extracted at the lower plate. Avg momentum density is  $\frac{1}{2}\rho V\hat{x}$ .

Momentum flux density =  $\Pi_{xz} = n \langle p_x v_z \rangle = \rho \langle v_x v_z \rangle$

is the drag force on the upper plate per unit area.

Note  $[\Pi_{xz}] = ML^{-3} \cdot (LT^{-1})^2 = ML^{-1}/T^2 = F/A$ .

This is given by  $\Pi_{xz} = -\eta \partial v_x / \partial z$  where  $\eta$  is the shear viscosity of the fluid. For a fluid in motion with constant velocity  $\vec{V}$ , we have

$$\begin{aligned}\Pi_{\alpha\beta} &= mn \langle (v_\alpha + v'_\alpha)(v_\beta + v'_\beta) \rangle \\ &= nm v_\alpha v_\beta + \frac{1}{3} nm \langle \vec{v}'^2 \rangle \\ &= \rho v_\alpha v_\beta + p \delta_{\alpha\beta}\end{aligned}$$

where  $p$  is the pressure. When  $\vec{V}$  is spatially varying,

$$\Pi_{\alpha\beta} = p \delta_{\alpha\beta} + \rho v_\alpha v_\beta - \tilde{\sigma}_{\alpha\beta}$$

where  $\tilde{\sigma}_{\alpha\beta} = \eta \left( \frac{\partial v_\alpha}{\partial x^\beta} + \frac{\partial v_\beta}{\partial x^\alpha} - \frac{2}{3} \vec{\nabla} \cdot \vec{V} \delta_{\alpha\beta} \right) + \zeta \vec{\nabla} \cdot \vec{V} \delta_{\alpha\beta}$

is the viscosity stress tensor. Note that the term

in green is  $2\eta(Q_{\alpha\beta} - \frac{1}{3}\text{Tr}Q\delta_{\alpha\beta})$  where

$$Q_{\alpha\beta} = \frac{1}{2} \left( \frac{\partial V_\alpha}{\partial x^\beta} + \frac{\partial V_\beta}{\partial x^\alpha} \right) \quad (\text{as above})$$

Thus  $\text{Tr} \tilde{\sigma}_{\alpha\beta} = 3\zeta \vec{\nabla} \cdot \vec{V}$ , where  $\zeta$  is the bulk viscosity. Within the RTA,

$$\delta f(\vec{p}) = -\frac{\tau}{k_B T} \left\{ m v_\alpha v_\beta Q_{\alpha\beta} + \frac{\epsilon - c_p T}{T} \vec{v} \cdot \vec{\nabla} T - \frac{k_B \epsilon}{c_v} \vec{v} \cdot \vec{v} \right\} f^0$$

Assuming  $\vec{\nabla} T = \vec{v} \cdot \vec{\nabla} = 0$ , we have

$$\begin{aligned} \Pi_{xz} &= n \int d^3 p p_x v_z \delta f(\vec{p}) = -\frac{n m^2 \tau}{k_B T} Q_{\alpha\beta} \langle v_x v_z v_\alpha v_\beta \rangle \\ &= -n \tau k_B T \left( \frac{\partial V_x}{\partial z} + \frac{\partial V_z}{\partial x} \right) \end{aligned}$$

need  $(\alpha, \beta) = (x, z)$   
or  $(z, x)$  if this  
is to be nonzero

Thus we conclude

$$\eta = n k_B T \tau = \frac{\pi}{8} n m l \bar{v} \propto T^{1/2}$$

Note that  $\eta(T)$  vanishes at  $T=0$ . Our intuition may say that a liquid should gum up at low  $T$ , as

it approaches a glass or crystallization transition. But our calculation is for gases, and in a regime where such physics is not relevant.

## Oscillating Force

Suppose the gas particles are subjected to an oscillating external force  $\vec{F}(t) = \vec{F} e^{-i\omega t}$  (real part thereof). We'll keep things simple and take

$\vec{\nabla} T = \partial_\alpha V_\beta = 0$ , in which case the BE in the RTA is

$$\frac{\partial \delta f}{\partial t} + \vec{F} e^{-i\omega t} \cdot \vec{v} \frac{\partial f^0}{\partial \varepsilon} = 0 \Rightarrow$$

$$\delta f(\vec{p}, t) = \frac{\tau e^{-i\omega t}}{1 - i\omega\tau} \frac{\partial f^0}{\partial \varepsilon} \vec{F} \cdot \vec{v}$$

Now compute the particle current:

$$j^\alpha(t) = \int d^3 p v^\alpha \delta f = \frac{\tau e^{-i\omega t}}{1 - i\omega\tau} \frac{F^\beta}{k_B T} \int d^3 p f^0(\vec{p}) v^\alpha v^\beta$$

$$= \frac{\tau e^{-i\omega t}}{1 - i\omega\tau} \cdot \frac{nF^\alpha}{3k_B T} \int d^3v P(\vec{v}) \vec{v}^2$$

and we arrive at

$$j^\alpha(t) = \frac{n\tau}{m} \cdot \frac{F^\alpha e^{-i\omega t}}{1 - i\omega\tau}$$

For electrical conductivity,  $j_e^\alpha = -e j^\alpha$  and  $F^\alpha = -eE^\alpha$ , so

$$j_e^\alpha(t) = \frac{ne^2\tau}{m} \frac{E^\alpha e^{-i\omega t}}{1 - i\omega\tau} = \sigma_{\alpha\beta}(\omega) E^\beta e^{-i\omega t}$$

where the frequency-dependent conductivity is

$$\sigma_{\alpha\beta}(\omega) = \frac{ne^2\tau}{m} \cdot \frac{1}{1 - i\omega\tau} \cdot \delta_{\alpha\beta}$$

For electrons we should use  $f^0(\vec{p}) = \frac{h^{-3}}{e\beta(\epsilon(\vec{p}) - \mu)}$

This affects the relation  $n = n(\mu)$ , but the above Drude formula remains unchanged.