

Notes 29.

→ Microscopic Origins of Viscosity

Non-Ideal Fluids, Transport, Chapman-Enskog (Viscous)

Applications of the Boltzmann Equation

- Chapman-Enskog \rightarrow Basis (C-E Light)
- a major application of B.E. is calculation of transport coeffs. Derived Fluid Eqs
- recall, fluid equations involve momentum, heat flux

i.e. really $\frac{\partial \underline{U}}{\partial t} = -\nabla \cdot \underline{\underline{\Pi}}$, etc.

continuity form

here:

$$\Pi_{\alpha\beta} = mn (u_\alpha v_\beta + \langle v'_\alpha v'_\beta \rangle) +$$

$$\langle v'_\alpha v'_\beta \rangle = \int d^3v f v'_\alpha v'_\beta$$

$$\text{if } f = f_{eq} = \frac{n(\alpha)}{(2\pi)^{3/2} v_{Th}(\alpha)^3} \exp\left[-\frac{(v-v(\alpha))^2}{2 v_{Th}^2}\right]$$

$$\Rightarrow \langle v'_\alpha v'_\beta \rangle = \frac{1}{3} \langle v^2 \rangle \delta_{\alpha\beta}$$

$$\langle v^2 \rangle = 3T/m$$

but ~~is~~ is $f = f_{eq}$? ?

Recall, f satisfies:

$$\partial_t f + \underline{v} \cdot \underline{\nabla} f = C(f)$$

f_{eq} is soln. to $C(f) = 0$.

$\Rightarrow f_{eq}$ cannot solve B.E. unless $\underline{\nabla} f_{eq} = 0$!

can assign time scales:

$$\partial_t f \rightarrow \omega$$

$$\underline{v} \cdot \underline{\nabla} f \rightarrow v_{th} / L$$

$$C(f) \rightarrow \nu$$

Collisional regime has $\nu > \frac{v_{th}}{L}$
 $d < \bar{r} < l_{mfp} < L$

$$\nu = \frac{v_{th}}{l_{mfp}} \quad \frac{v_{th}}{L} < \nu$$

$$l_{mfp} = \lambda / nT$$

$\Rightarrow f_{eq}$ is 0th order solution.

then if f_0 is homogeneous \Rightarrow

stationary solution has correction!

$$f = f_0 + \delta f$$

$\hookrightarrow \sim$ inhomogeneity b i.e. $\nabla T, \nabla V$

more precisely response to inhomogeneity

$$\text{and } \langle \underline{v}'_A \underline{v}'_B \rangle = \int d^3v (f_0 + \delta f) v'_A v'_B$$

$$= \rho \alpha_{A,B} + \text{viscous stress}$$

$$\sim \nabla V$$

stress vs. rate strain.

viscosity $\sim \mu D$

d.e. $\mu \langle v'_x v'_y \rangle_{visc} = -\eta \frac{\partial \langle v_x \rangle}{\partial x}$ + ... $D \sim \text{length}$

so, need:

general form of viscous stress

- understand viscosity, etc.

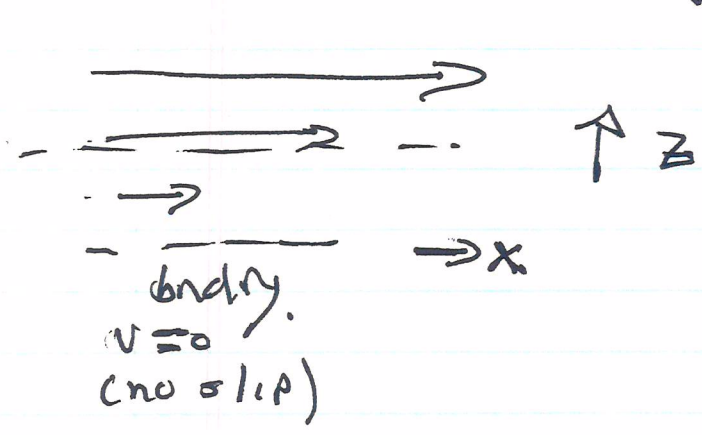
Flux-Gradient

- see how calculate dF and then transport coeffs (viscosity)

so what is viscosity about?

- sample physics of transport coeffs!

Consider collisional gas:

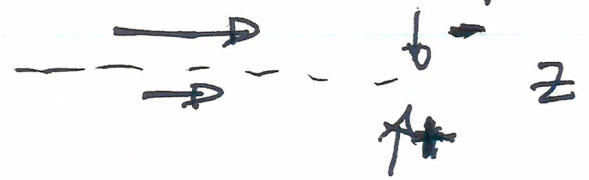


mean flow

$v = v(z) \hat{x}$

i.e. shear flow (gradient \perp flow)

choose imaginary surface:



Calculate transport of \vec{x} momentum thru surface:

$$\pi_+ = \int_{v_z > 0} d\underline{v} m v_x v_z f$$

$$\sim v_{Tn} \bar{V} n m_+$$

$$\pi_- = \int_{v_z < 0} d\underline{v} m v_x v_z f$$

at first glance, would appear $\pi_+ = \pi_-$

so $\pi_{tot} = 0$?! but ! :

— — — — \Rightarrow  mesh

\rightarrow "scale of resolution" for imaginary surface is $l_{mp} \Rightarrow$ defines effective thickness.

\rightarrow "V(z) has gradient across this!"

$$\stackrel{\infty}{=} \pi_{tot} = \pi_- + \pi_+$$



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 π_-

$$\pi \approx -n m v_{Th} \bar{V} \left(z + \frac{l_{mp}}{2} \right) + n m v_{Th} \bar{V} \left(z - \frac{l_{mp}}{2} \right)$$

 π_+ expansion
smooth V

$$\approx -n m v_{Th} l_{mp} \frac{\partial V}{\partial z}$$

$\rightarrow \sim l_{mp} v_{Th}$

$$\approx -n m D \frac{\partial V}{\partial z}$$

$$= -\eta \frac{\partial V}{\partial z}$$

viscosity (shear)

$$\sim \rho D$$

$$D \sim v_{Th} \tau$$

→ Key Points:

- equal # collisions, kicks in t_1 - direction, but

- more momentum kicked down from above, due velocity gradient.

→

- net viscous momentum transport via collisions, to relax gradient

How calculate systematically?

⇒ Chapman - Enskog expansion!

now

$$\frac{df}{dt} + \underbrace{v \cdot \nabla}_\downarrow \underbrace{f}_\downarrow = \underbrace{CCE}_\downarrow$$

$\frac{v_{Th}}{L}$ $v_{eff.}$ $v > \frac{v_{Th}}{L}$

{ multiple times scales
F normalization

and see k:

$$\Pi_{z,x} = \int d^3v \cdot v_z (m v_x f)$$

\downarrow
 \hat{z} direction flux of \hat{x} momentum

$$f = f_0 + df$$

$$\Pi_{z,x} = \int d^3v \cdot v_z (m v_x (f_0 + df))$$

if $f_0 \approx \frac{n_0}{v_{Th}^3} \exp\left[-\frac{(v - v(z)\hat{x})^2}{2 v_{Th}^2}\right]$

(i.e. local Maxwellian)

→ For contribution vanishes by symmetry!

so

$$\Pi_{z,x} = \int d^3x v_z (m \cancel{v_x}) \delta f$$

↑
drives the flux.

How get δf ?

⇒ Perturbative solution!

$$\nabla \cdot \delta f = C(\delta f) \rightarrow \left\{ \begin{array}{l} \text{really an} \\ \text{integral} \\ \text{equation!} \end{array} \right.$$

$$\text{e. o. : } C(\delta f) = 0$$

$$f = f_0 \rightarrow \underline{\text{Local Maxwellian}}$$

1st o. :

$$\nabla \cdot \nabla f_0 = C(\delta f)$$

$$\therefore \delta f = C^{-1} [\nabla \cdot \nabla f_0]$$

How?

→ lengthy calculation ~~XXXXXXXXXX~~

→ Krook (Crock) Model !

$$C(f) = -\nu (f - f_{eq})$$

collisional decay to
(local) Maxwellian
coset Empty

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$$\underline{v} \cdot \underline{\nabla} f = C(f) = -\nu (f - f_{eq})$$

$$f = f_{eq} + \delta f$$

$$\underline{v} \cdot \underline{\nabla} (f_{eq} + \delta f) = -\nu (f - f_{eq})$$

$$\text{l.o. : } -\nu (f - f_{eq}) = 0$$

$$f = f_{eq}$$

1st order :

$$\underline{v} \cdot \underline{\nabla} f_{eq} = -\nu \delta f$$

$$\delta f = - \frac{\underline{v} \cdot \underline{\nabla} f_{eq}}{\nu}$$

perturbative
correction to f_{eq} ; $O\left(\frac{v_{th}}{L\nu}\right)$

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$$\begin{aligned} \Pi_{2,x} &= \int d^3v v_z m v_x dF \\ &= \int d^3v v_z n m v_x \left(-\frac{v_z}{r} \frac{\partial}{\partial z} f_{e1} \right) \end{aligned}$$

$$V_{\vec{x}} = V(z) \vec{x}$$

$$\begin{aligned} \text{now } f_{e1} &\approx \frac{n(x)}{V_{th}(x)} \exp \left[-\frac{(v - V(z) \vec{x})^2}{2 V_{th}^2(x)} \right] \\ &= \frac{n}{V_{th}^3} \exp \left[-\frac{(v - V(z))^2}{2 V_{th}^2} \right] \end{aligned}$$

$$\begin{aligned} \frac{\partial f_{e1}}{\partial z} &= \frac{n}{V_{th}^3} \frac{v_x}{V_{th}^2} \frac{\partial V(z)}{\partial z} \exp \left[\dots \right] \\ &\quad - 2 \frac{V(z)}{V_{th}^2} \frac{\partial V(z)}{\partial z} \exp \left[\dots \right] \end{aligned}$$

linear response.

dropped \Rightarrow
interested in only
linear response
of flux to
gradient.

see next

$$\frac{\partial f_0}{\partial z} = f_{e1} \frac{v_x}{V_{th}^2} \frac{\partial V(z)}{\partial z}$$

~~... ..~~
~~... ..~~
~~... ..~~
~~... ..~~

Note:

→ here seek linear relation between flux and gradient

→ presumes weak distortion from Maxwellian, i.e.

$$f_{\text{eq}} = \frac{n}{V_{\text{th}}^3} \exp \left[-\frac{(v - v_D)^2}{2V_{\text{th}}^2} \right]$$

$$= \frac{n}{V_{\text{th}}^3} \exp \left[-\frac{(v^2 - 2v v_D + v_D^2)}{2V_{\text{th}}^2} \right]$$

$$\approx \frac{n}{V_{\text{th}}^3} \exp \left[-\frac{v^2}{2V_{\text{th}}^2} \right] \left[1 + \frac{v v_D}{V_{\text{th}}^2} \right]$$

$$= f_{\text{eq}}^0 \left(1 + \frac{v_x v_D}{V_{\text{th}}^2} \right)$$

↑
e.o. factor on expansion

yields result.

4p-coming → "Linear Response Theory"

Green-Kubo Relation

$$\Pi_{zx} = \int d^3x \frac{1}{2} m v_x \left(-\frac{v_z}{r} \frac{v_x}{v_{Th}^2} \right)$$

$$\propto \frac{1}{2} m n \frac{\partial V(z)}{\partial z}$$

$$= -\frac{1}{2} m n \frac{v_{Th}^2}{r} \frac{\partial V(z)}{\partial z}$$

$$= -\frac{1}{2} m n \left(\frac{v_{Th}}{r} \right) v_{Th} \frac{\partial V(z)}{\partial z}$$

↳
length

$$D = v_{Th} \text{ length}$$

$$\Pi_{zx} = -\frac{1}{2} m n D \frac{\partial V(z)}{\partial z}$$

$$= -\frac{1}{2} \rho D \frac{\partial V(z)}{\partial z}$$

$$\eta = -\frac{1}{2} \rho D$$

⇒ basic result for collisions) shear viscosity

can get #

Note form of result:

$$\Pi_{zx} = - \underbrace{\# n m D}_{\text{microscopic}} \frac{\partial V_x(z)}{\partial z}$$

\downarrow
 transport coefficient

\hookrightarrow gradient of thermo. quantity (dist.)
 \downarrow
 thermodynamic force.

\downarrow
 Flux

\Rightarrow example of thermodynamic

~~flux-force relation.~~

\Rightarrow constitutive relation. proportionality is transport coefficient

In general, have vector relation:

$$\underline{\Gamma} = - \underline{L} \cdot \underline{\nabla} C$$

\downarrow
 vector of fluxes

\downarrow
 vector of gradients

\downarrow
 matrix of transport coefficients - Onsager matrix
 (n.b. Onsager symmetry \rightarrow L symmetric)

⇒ Observe:

- F_{Max} annihilates collision operator,

and corresponds to $\frac{dS}{dt} = 0$

state → maximal entropy.

but

- $f_{\text{Max}} [n(x), T(x), V(x)]$ does not satisfy Boltzmann eqn. ⇒ df needed.

i.e. $\nabla \cdot \mathbf{D} f = c(f)$

⇒ $F = f_{\text{Max}} + df$

Why?

→

gradients in thermodynamic quantities ⇒ system is not in maximum entropy state
i.e. $df \neq 0$

- so $df \sim \nabla C$, ⇒ relaxation to maximum entropy state will occur by collisions / transport.

- can describe relaxation macroscopically, i.e.

$$\underbrace{\Pi_{\alpha, \beta}}_{\text{flux}} = -\rho D \underbrace{\frac{\partial V_{\beta}}{\partial x_{\alpha}}}_{\text{force}} \quad \frac{\partial \rho v}{\partial t} = -\rho \cdot \underline{\underline{\Pi}}$$

$$-\frac{\partial V_{\beta}}{\partial x_{\alpha}} \Pi_{\alpha, \beta} = \rho D \left(\frac{\partial V_{\beta}}{\partial x_{\alpha}} \right)^2 \quad \int \epsilon_{\text{th}} = \int \Pi \cdot \underline{dv}$$

$$\boxed{\frac{dS}{dt} = \frac{\rho D}{T} \left(\frac{\partial V_{\beta}}{\partial x_{\alpha}} \right)^2}$$

- entropy production due transport
- induced relaxation

Note time scales:

i.) to form local Maxwellian, H-thm. $\Rightarrow \tau_{\text{coll}} \sim \nu^{-1}$

ii.) to form global ~~maximum~~ ^{maximum} entropy state:

$$\frac{1}{\tau_{\text{relax}}} \sim \frac{D}{L^2} \sim \nu \frac{L_{\text{mix}}^2}{L^2}$$

$$L_{\nu}^{-1} = \frac{D}{\nu} \frac{\partial V}{\partial x}$$

$$\tau_{relax} \sim \left(L_V / l_{MFP} \right)^2 \tau_{coll}$$

⇒ entropy production / relaxation is multiple time scale process!

More generally, can write:

$$J_i = - \sum_{j=1}^n \alpha_{ij} X_j$$

α_{ij} kinetic coefficient \rightarrow driving force
 J_i i-th flux

$$\frac{dS}{dt} = \psi = \text{"Dissipation Function"}$$

$$\Rightarrow \frac{dS}{dt} = \sum_{i=1}^n \sum_{j=1}^n \alpha_{ij} X_i X_j$$

$\alpha_{ij} = \alpha_{ji}$
 if basic interaction time reversible.
 Onsager Symmetry

i.e. $\frac{dS}{dt} = - \sum_j X_j J_i$

so, for 2x2:

$$\frac{dS}{dt} = \sum_{i=1}^2 \sum_{j=1}^2 \alpha_{ij} X_i X_j = \alpha_{11} X_1^2 + (\alpha_{12} + \alpha_{21}) X_1 X_2 + \alpha_{22} X_2^2$$

clearly need:

$$\begin{array}{l} \alpha_{1,1} \geq 0 \\ \alpha_{2,2} \geq 0 \end{array} \rightarrow \text{i.e. diffusion down gradient}$$

and $\alpha_{1,1} \alpha_{2,2} - \frac{1}{4} (\alpha_{1,2} + \alpha_{2,1})^2 \geq 0.$

(i.e. det \rightarrow disc.)

N.B. OFF-diagonals!

i.e. Can ∇T drive a density flux?

$$\Gamma = \int d^3v \mathbf{v} \sigma f$$

$$\sigma f = -\frac{1}{T} \mathbf{v} \cdot \nabla f_0$$

$$\Rightarrow \Gamma = \int d^3v \mathbf{v} \cdot \left(-\frac{1}{T} \mathbf{v}_x \frac{\partial}{\partial x} \left(\frac{n_0}{v_{th}^3} \exp\left[-\frac{mV^2}{2T(x)}\right] \right) \right)$$

clearly can get contribution to Γ_x .
 \rightarrow Thermal diffusion.

Message: Gradient in distribution function is the key! ... but integration symmetric matter.